

explored medium, that is to say a medium subjected to ultrasound signals emitted and received by an echography apparatus. The invention is based on the processing of the echographic signal in order to determine the distribution of the elasticity modulus in the explored medium while using a regularized inverse solving method, applied to data of a field of displacements measured in said medium. The invention can be very attractively applied for the detection of malignant tumors by determination of the distribution of the elasticity modulus in the tissues, as well as for the determination of the size of such tumors.

The medium in FIG. 1 is, by way of example, breast tissue which is called texture 11. A continuously variable pressure P is applied to the breast tissue and a displacement field is determined by subjecting a region of the tissue to ultrasound signal excitations and by applying a correlation method to the ultrasound signals. More specifically, the pressure P continuously increases and is applied by means of a compressor 12 which is driven by a motor 13. The zone 11 of the breast tissue which is subjected to the compression has a fixed face F1 whereto a probe 10 of an echography apparatus 100 is applied, and a parallel face F2 whereto the pressure P of the compressor is applied in the perpendicular direction. In the device according to the invention as shown in FIG. 1, the mobile wall of the compressor 12 applied to the face F2 is displaced in the direction of the face F1 at a given speed \vec{v} . The probe 10 applied to the fixed face F1 applies RF signals to the texture 11 during excitations parallel to the direction of the face F2. The excitation lines along the axis Z extend perpendicularly to the faces F1 and F2 and parallel to the direction of the pressure of the compressor 12. The excitations are produced by the echography apparatus 100 which includes a system 110 for focusing the RF signals in the tissue 11, parallel to an axis Z, and for scanning by way of the excitation signals RF linearly parallel to an axis X which extends parallel to the face F1. The scanning according to the axis X is performed along a given number of N excitation lines with a recurrent period T. When the N excitations from 1 to N parallel to Z have been performed, the probe starts anew with N excitations from 1 to N with a period NT for a given excitation line. The probe in return receives from the texture 11 the echographic signals which are applied to an elasticity variation detection system 200. Preferably, the probe consists of an array of linear detectors emitting recurrent excitations. The system 200 includes a 1-bit temporal correlation system 210 for performing in real time the correlation of each of the signals transmitted by the probe and originating from a given location in the texture 11. The correlation system 210 executes the correlation of signals relating to two successive excitations of the probe and originating from a given location, and provides the amplitude of the displacements of each point of the structure 11 explored by the probe on each excitation line. During the operation of the compressor 12, this method supplies, continuously and in real time, an image of the displacement field of the structures forming the texture 11.

To this end, the image of the displacement field in the zone of the explored texture 11 is discretized. The signals produced by the various scans by the probe are not stored. These signals are correlated directly by the 1-bit temporal correlation system 210 which provides an image of the displacements of each point of the structure, for example in the form of iso-displacement lines as illustrated in FIG. 3. The present method also involves specific means for making the determination of the distribution of the elasticity modulus distribution resistant to noise in order to realize, in combination with a reconstruction of the elasticity modulus

distribution which is realized in real time, a reconstruction which is less noisy than that achieved according to the state of the art.

It is to be noted that the displacements calculated by the correlation system 210 result from direct measurements of the displacements of the structures of the region explored by means of the echography apparatus. These displacements are radial, parallel to the pressure P and are obtained under the influence of said external pressure P exerted on the tissue 11.

Preferably, several series of scans are performed while using therebetween an equal compression or a displacement, equal to $\vec{v} \times NT$, of the face F2 of the compressor, followed by averaging of the data supplied by the correlation system 210. This method enables a high precision to be achieved in this step 210 for the acquisition of the displacement field.

In the step 210 the data of the displacement field is calculated in the form of elementary displacements $d_1, \dots, d_p, \dots, d_n$ for each pixel of the discretized ultrasonic image obtained by way of the correlation method. The data of the elementary displacements constitutes a displacement data vector \underline{d} .

This displacement vector \underline{d} is linked to a so-called elasticity modulus vector (or Young modulus) \underline{e} by a direct relation F which is written as (1):

$$\underline{d} = F(\underline{e}) \quad (1)$$

The elasticity modulus vector \underline{e} is formed by elementary elasticity moduli $e_1, \dots, e_p, \dots, e_n$ which correspond to the respective elementary displacements relating to each pixel p_1, \dots, p_p, p_n of the discretized image. It is known that $F(\underline{e})$ is the image realized by means of a Finite Element Model of the distribution of the elementary elasticity moduli, that is to say of the vector \underline{e} . A Finite Element Model is a calculation technique which can be applied to the elasticity equations and is known to those skilled in the art.

The problem to be effectively solved is the determination of the vector \underline{e} giving the distribution of the elasticity modulus in the explored region having produced the displacement field. The determination of the vector \underline{e} enables the formation of an image of the elasticity modulus distribution which is formed by elementary moduli relating to each pixel of the discretized image.

The value of the vector \underline{e} is obtained, on the basis of the relation (1), by solving the inverse problem according to the relation (2):

$$\hat{e} = \arg \min [\|\underline{d} - F(\underline{e})\|^2] \quad (2a)$$

where \hat{e} is an estimator of \underline{e} . The estimator \hat{e} of the elasticity modulus \underline{e} minimizes the distance $\|\underline{d} - F(\underline{e})\|^2$ between the data \underline{d} acquired by means of the measurements in the step 210 of FIG. 1 and the image $F(\underline{e})$ realized by means of the Finite Element Model. The estimator \hat{e} enables determination of the vector \underline{e} which, once it has been inserted into the Finite Element Model, yields a value of the vector \underline{d} which approximates as closely as possible the vector \underline{d} measured in the step 210.

The relation (2a) is known from the publication cited as the state of the art and is called the Newton-Raphson algorithm. This algorithm enables calculation of the minimum value of the distance $\|\underline{d} - F(\underline{e})\|^2$ in an iterative manner, for example by means of 10 or 15 iterations according to the state of the art. The Newton-Raphson algorithm utilizes an iterative minimization of the distance which is written as: